

5/13

DART AEROSPACE LTD	Work Order:	22527
Description: Arm	Part Number:	D3387-041
Dwg: D3387 Rev. A	Qty:	40
		Page 1 of 1

Step	Location	Procedure	By	Date	Qty
1	DC	Issue Traveler	JS	05.02.23	40
2	MV	Cut blank: 6.000" x 0.500" x 17.800" long Material: 6061-T6/T651 (QQ-A-200/8) (M6061T6B0.500x06.000) Identify for D3387-1	M16991 M16953 Batch: M16764 E	05.02.23	40
3	MV	Machine as per Folio FA511 and Dwg D3387 Identify as D3387-1	E / J.L	07-3-05	40
4	MV	C'sink Ø0.375" as per Dwg D3387	E	05.03.05	40
5	QC2	Inspect parts as they come off the CNC machine	E / J.L	07-3-05	40
6	QC8	Second check	ML	05/03/07	40
7	MV	Tumble and Deburr NO sharp edges	E / J.L	05-03-07	40
8	QC5	Inspect work to Step 7	ML	05/03/07	40
9	FP	Chemical Conversion Coat as per QSI 005 4.1			
10	QC3	Inspect Chemical Conversion Coat			
11	GA	Press spacer into D3387-1 arm as per Dwg D3387 Pick: Qty Part Number Description Batch 1 D2808 Spacer			
12	QC5	Inspect work to Step 11			
13	ST	Identify and Stock	PD	05.03.08	40
14	AC	Cost / part: 29.75	SAC	05.03.09	40
15	DC	Close W/O 29.75 Inspect Level 21	LD	05/09/19	40

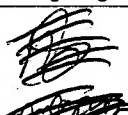
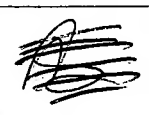

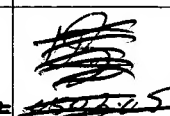
Not Applicable for this work

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Rev	Date	Change	Revised By	Approved
A	05.02.22	New Issue	KJ/JLM	

RELEASED
11/03/23

W/O:		WORK ORDER CHANGES					
DATE	STEP	PROCEDURE CHANGE	By	Date	Qty	Approval Mfg / Design Mgr	Approval QC Inspector

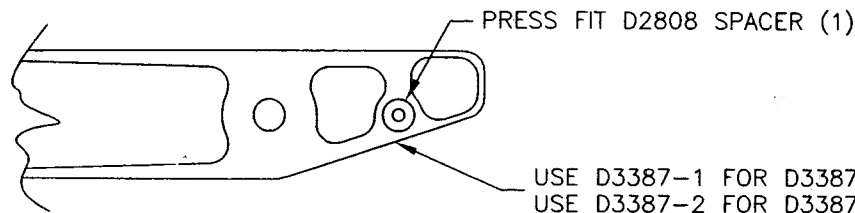
NCR:		WORK ORDER NON-CONFORMANCE (NCR)						
DATE	STEP	Description of NC Section A	Corrective Action Section B			Verification Section C	Approval Design Mgr	Approval QC Inspector
			Initial Design Mgr	Action Description Design Mgr	Sign & Date			
05-07-03	3	- 1 part is under tol, by 0.005" on 2.000 dim. should be 2.000 ^{+0.01} _{-0.005} reading 1.990"	 CP	PART IS ACCEPTABLE. MARGIN IS STILL POSITIVE.			 05.08.12	

Part No: _____ PAR #: _____ Fault Category: _____ NCR: Yes ☒ No ☐ DQA:  Date: 05/09/19

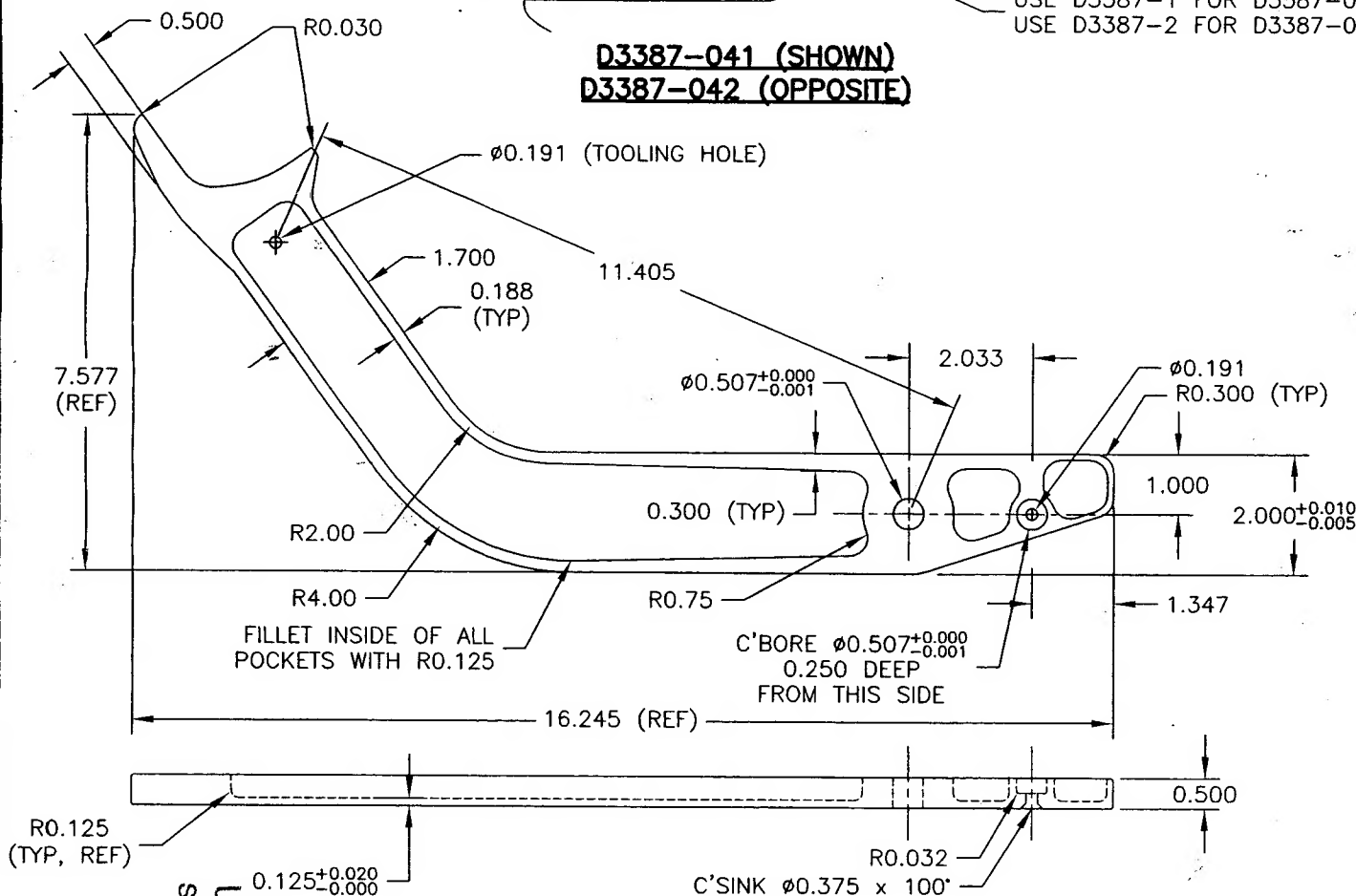
NOTE: Date & initial all entries QA: N/C Closed: _____ Date: _____

PRELIMINARY ISSUE

DESIGN	00	DRAWN BY	00	DART AEROSPACE LTD HAWKESBURY, ONTARIO, CANADA
CHECKED		APPROVED		DRAWING NO. D3387
DATE	05.01.18	TITLE	ARM	REV. A SHEET 1 OF 1
A	05.01.18	NEW ISSUE		SCALE 1:3



D3387-041 (SHOWN)
D3387-042 (OPPOSITE)



D3387-1 (SHOWN)
D3387-2 (OPPOSITE)

GENERAL NOTES

- (1) MACHINE PER DRAWING FILE "D3387-A.DWG"
- (2) MATERIAL 6061-T6 (QQ-A-200/8 OR QQ-A-250/11) 0.500 THICK (REF DART SPEC. M6061T6B0.500)
- (3) DEBURR TO LEAVE R0.030 - 0.063 ON ALL EDGES
- (4) TOLERANCES ARE PER DART QSI 018 UNLESS OTHERWISE NOTED
- (5) ALL DIMENSIONS ARE IN INCHES

WORK ORDER

NO. 22527

Job Costing Report

Dart Aerospace Ltd.
Hawkesbury

Feb 22, 2005
03:39 pm

Work Order No : 0022527
Project Name : D3387-041
Project For : WK513
Work Order Type : Main
Main WO Number :
House Part Number : D3387-041
Description : Arm Assembly
Manufactured : No
Amount Req'd : *0*
Amount Done : 0
Start Date : 02-22-05
Est Finish Date : 03-15-05
Act Finish Date :
Drawings Req'd : No
Ok for Approval :
Approval Rec'd :

Department Code:
Burden Flags : NNNNNNNN
WO Status : Open
Invoice State : Not Invoiced
Invoice Date :
Invoice Number :
Invoice Amount : 0.00
Order Entry No :
OE Value : 0.00
Est Margin : 0.000%
Actual Margin : 0.000%
\$0 Posted to Finished Goods

	Estimated	Actual	Var. %	Posted	To Post
Material Cost :	0.00	0.00	0.00	0.00	0.00
Engineering Hours :	0.00	0.00	0.00		
Engineering Cost :	0.00	0.00	0.00	0.00	0.00
Production Hours :	0.00	0.00	0.00		
Production Cost :	0.00	0.00	0.00	0.00	0.00
Packaging Hours :	0.00	0.00	0.00		
Packaging Cost :	0.00	0.00	0.00	0.00	0.00
OverHead Hours :	0.00	0.00	0.00		
OverHead Cost :	0.00	0.00	0.00	0.00	0.00
CNC Hours :	0.00	0.00	0.00		
CNC :	0.00	0.00	0.00	0.00	0.00
Misc. Hours :	0.00	0.00	0.00		
Misc. :	0.00	0.00	0.00	0.00	0.00
Burden :	0.00	0.00	0.00		
Total Cost :	0.00	0.00	0.00		
Margin :	0.000	0.000			
Selling Cost :	0.00	0.00			

	Estimated	Actual
Labour Hrs/Amount Done :	0.00	0.00
Profits/(Loss) :	0.00	0.00

6.2 D3387-1/-2 ARM

The D3387-1/-2 arms are used in the D412-630-023/-024 steps. The maximum load in this part corresponds to R84L = R155L determined in section 4.1 of this report. Refer to Figure 6 in Appendix D for the geometry involved in this analysis. For each critical section shown in Figure 6, the D3387-1/-2 arms are checked for bending failure.

Geometry

$$\begin{aligned} x1 &:= 12.19 \cdot \text{in} & x_a &:= 11.64 \cdot \text{in} & \theta_a &:= 35.77 \cdot \text{deg} \\ x2 &:= 1.99 \cdot \text{in} & x_b &:= 0.95 \cdot \text{in} \\ & & x_c &:= 0.60 \cdot \text{in} \\ & & x_d &:= 6.21 \cdot \text{in} \end{aligned}$$

Loads

$$\begin{aligned} F &:= R84L & F &= 765 \cdot \text{mass} & \text{Applied load} \\ M_{\text{max}} &:= F \cdot x1 & M_{\text{max}} &= 9325 \cdot \text{lb} \cdot \text{in} & \text{Maximum bending moment} \\ F_s &:= \frac{M_{\text{max}}}{x2} & F_s &= 4686 \cdot \text{mass} & \text{Load applied to the stop} \\ F_{py} &:= F + F_s \cdot \sin(\theta_a) & F_{py} &= 3504 \cdot \text{mass} & \text{Vertical load at the pivot} \\ F_{px} &:= F_s \cdot \cos(\theta_a) & F_{px} &= 3802 \cdot \text{mass} & \text{Horizontal load at the pivot} \\ F_p &:= \sqrt{F_{py}^2 + F_{px}^2} & F_p &= 5171 \cdot \text{mass} & \text{Total pivot load} \end{aligned}$$

Section A-A Analysis

$$\begin{aligned} H &:= 1.99 \cdot \text{in} \quad t := 0.125 \cdot \text{in} \quad w := 0.50 \cdot \text{in} \quad h := 0.295 \cdot \text{in} & \text{Section A-A parameters} \\ I &:= \frac{t \cdot H^3}{12} + 2 \cdot \left[\frac{(w - t) \cdot h^3}{12} + (w - t) \cdot h \cdot \left(\frac{H}{2} - \frac{h}{2} \right)^2 \right] & I = 0.243 \cdot \text{in}^4 & \text{Inertia at Section A-A} \\ M_a &:= \frac{x_a}{x1} \cdot M_{\text{max}} & M_a &= 8905 \cdot \text{lb} \cdot \text{in} & \text{Moment at Section A-A} \\ \sigma_a &:= \frac{M_a \cdot H}{2 \cdot I} & \sigma_a &= 36520 \cdot \text{psi} & \text{Stress at Section A-A} \\ MS_{23a} &:= \frac{F_{tu}}{\sigma_a} - 1 & MS_{23a} &= 0.04 & \text{Margin of Safety at Section A-A} \end{aligned}$$

Section B-B Analysis

$$\begin{aligned} H &:= 1.744 \cdot \text{in} \quad t := 0.125 \cdot \text{in} \quad w := 0.50 \cdot \text{in} \quad h := 0.25 \cdot \text{in} & \text{Section B-B parameters} \\ I &:= \frac{t \cdot H^3}{12} + 2 \cdot \left[\frac{(w - t) \cdot h^3}{12} + (w - t) \cdot h \cdot \left(\frac{H}{2} - \frac{h}{2} \right)^2 \right] & I = 0.161 \cdot \text{in}^4 & \text{Inertia at Section B-B} \\ M_b &:= \frac{x_b}{x2} \cdot M_{\text{max}} & M_b &= 4452 \cdot \text{lb} \cdot \text{in} & \text{Moment at Section B-B} \\ \sigma_b &:= \frac{M_b \cdot H}{2 \cdot I} & \sigma_b &= 24133 \cdot \text{psi} & \text{Stress at Section B-B} \\ MS_{23b} &:= \frac{F_{cy}}{\sigma_b} - 1 & MS_{23b} &= 0.409 & \text{Margin of Safety at Section B-B} \end{aligned}$$